



Buckling Analysis of Unidirectional Polymer Matrix Composite Plates

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Abstract:-

This study deals with the estimation of critical load of unidirectional polymer matrix composite plates by using experimental and finite element techniques at different fiber angles and fiber volume fraction of the composite plate.

Buckling analysis illustrated that the critical load decreases in nonlinear relationship with the increase of the fiber angle and that it increases with the increase of the fiber volume fraction.

The results show that the maximum value of the critical load is (629.54 N/m) at ($\theta = 0^\circ$) and ($V_f = 40\%$) for the finite element method, while the minimum value of the critical load is (49 N/m) at ($\theta = 90^\circ$) and ($V_f = 10\%$) for the experimental results.

The results also indicated that the maximum difference between the finite element analysis and experimental work is about (11 %) at ($\theta = 0^\circ$) and ($V_f = 40\%$).

1.Introduction

Many aeroengine components consist of thin-walled plates under loads which can potentially cause failure by buckling. These loads comprise combinations of compressive, shear and bending force [1].

The word "buckling" evokes an image of failure of structures which has been compressed in some way. Pictures and perhaps sound come to mind of sudden, catastrophic collapse involving very large deformations [2].

When the magnitude of the load on a structure is such that the equilibrium is changed from stable to

unstable the load is called a critical load (or buckling load) [3].

The nature of the buckle pattern in plate depends not only upon the type of the applied loading but also upon the manner in which the edges are supported, shape (dimension) of the problem and material properties.

The composite plate used in this study was a unidirectional polymer matrix composite plate made from glass fiber – epoxy matrix composite with constant length to width ratio ($L/w = 2$) at different fiber angles and fiber volume fraction.

The aim of this work is to investigate the buckling analysis of the

composite plate by using the finite element analysis and the experimental work.

An enormous amount of effort has been exerted on the subject of buckling since the beginning of the 20th century mainly the work performed by NACA (National Advisory Committee for Aeronautics).

Rais-Rohani, M and Marcellier, P. [4,5] studied the effects of elastic edge conditions, aspect ratio, and face sheet ply pattern on the buckling loads and natural frequencies of anisotropic rectangular sandwich plates by using Rayleigh – Ritz method.

Timothy L.C. Chen and Charles W. Bert [6] used the theory for buckling of laminated, anisotropic, thin plates to study buckling of the rectangular plates, laminated of composite material and subject to uniaxial compressive loading for optimal design plates laminated of glass/epoxy, boron/epoxy, and carbon/epoxy composite materials.

Hyonny Kim and Keith T. Kedward [7] studied the global buckling and local sublaminar buckling of the laminated plate containing Zone of delamination by using Rayleigh – Ritz method and finite element models.

Timoshenko, Stephen P. and James M. Gere [8] explained the approximate method to obtain the results of buckling stresses which are always higher than the exact solution.

Yasui [9] presented what appears to be the first in-depth parametric study of buckling behavior of laminated composite plates with a central circular cutout that has been obtained by using the finite element method.

Rouse [10] presented an experimental investigation of the buckling and postbuckling behavior of square graphite-epoxy and graphite-thermoplastic plates loaded in shear.

2.Theoretical Analysis

Using lamination theory, the strains in structural laminate resulting from a given applied stress from information on the basic lamina which are: glass and epoxy moduli, poisson's ratios, densities, and volume fractions of fibers, in addition to geometric data for the composite plate.

The constitute relations may be established for a lamina by assuming that the lamina is a homogeneous orthotropic material in a state of plane stress. The geometry of a single filamentary lamina is shown in figure (1) [11].

Hook's law for a composite material with orthotropic properties in a plane stress state is:

$$\begin{bmatrix} \sigma_1 \\ \sigma_2 \\ \tau_{12} \end{bmatrix} = \begin{bmatrix} Q_{11} & Q_{12} & 0 \\ Q_{21} & Q_{22} & 0 \\ 0 & 0 & Q_{33} \end{bmatrix} \cdot \begin{bmatrix} \varepsilon_1 \\ \varepsilon_2 \\ \gamma_{12} \end{bmatrix} \quad (1)$$

The components of the reduced stiffness matrix, [Q]. are:

$$Q_{11} = E_{11} / (1 - \nu_{12}\nu_{21}) \quad (2)$$

$$Q_{12} = Q_{21} = \nu_{21} \cdot E_{11} / (1 - \nu_{12} \cdot \nu_{21}) \quad (3)$$

$$Q_{33} = G_{12} \quad (4)$$

And the longitudinal and lateral elastic modulus is predicted by the rule of mixtures formula.

$$E_1 = E_f \cdot V_f + E_m \cdot V_m \quad (5)$$

$$E_2 = \frac{E_f \cdot E_m}{E_f \cdot V_m + E_m \cdot V_f} \quad (6)$$

And the major poisson's ratio is given by:-

$$\nu_{12} = \nu_f \cdot V_f + \nu_m \cdot V_m \quad (7)$$

And the minor poisson's ratio ν_{21} can be estimated from

$$\nu_{21} = \nu_{12} \cdot \frac{E_2}{E_1} \quad (8)$$

For a given fiber angle (θ) the stress/strain relationship

$$\begin{bmatrix} \sigma_x \\ \sigma_y \\ \tau_{xy} \end{bmatrix} = \begin{bmatrix} \bar{Q}_{11} & \bar{Q}_{12} & \bar{Q}_{13} \\ \bar{Q}_{21} & \bar{Q}_{22} & \bar{Q}_{23} \\ \bar{Q}_{31} & \bar{Q}_{32} & \bar{Q}_{33} \end{bmatrix} \cdot \begin{bmatrix} \varepsilon_x \\ \varepsilon_y \\ \gamma_{xy} \end{bmatrix} \quad (9)$$

$$\begin{aligned} \bar{Q}_{11} &= Q_{11} \cdot \cos^4 \theta + 2 \cdot (Q_{12} + 2Q_{33}) \cdot \sin^2 \theta \cdot \cos^2 \theta + Q_{22} \cdot \sin^4 \theta \\ \bar{Q}_{22} &= Q_{11} \cdot \sin^4 \theta + 2 \cdot (Q_{12} + 2Q_{33}) \cdot \sin^2 \theta \cdot \cos^2 \theta + Q_{22} \cdot \cos^4 \theta \\ \bar{Q}_{12} &= \bar{Q}_{21} = (Q_{11} + Q_{22} - 4 \cdot Q_{33}) \cdot \sin^2 \theta \cdot \cos^2 \theta + Q_{12} \cdot (\sin^4 \theta + \cos^4 \theta) \\ \bar{Q}_{33} &= (Q_{11} + Q_{22} - 2 \cdot Q_{12} - 2 \cdot Q_{33}) \cdot \sin^2 \theta \cdot \cos^2 \theta + Q_{33} \cdot (\sin^4 \theta + \cos^4 \theta) \\ \bar{Q}_{13} &= \bar{Q}_{31} = (Q_{11} - Q_{12} - 2 \cdot Q_{33}) \cdot \sin \theta \cdot \cos^3 \theta + (Q_{12} - Q_{22} + 2 \cdot Q_{33}) \cdot \sin^3 \theta \cdot \cos \theta \\ \bar{Q}_{23} &= \bar{Q}_{32} = (Q_{11} - Q_{12} - 2 \cdot Q_{33}) \cdot \sin^3 \theta \cdot \cos \theta + (Q_{12} - Q_{22} + 2 \cdot Q_{33}) \cdot \sin \theta \cdot \cos^3 \theta \end{aligned}$$

Also the stress/strain equation in the ply can be written in reference to the geometric midplane as follows:

$$\begin{bmatrix} \sigma_x \\ \sigma_y \\ \tau_{xy} \end{bmatrix} = \begin{bmatrix} \bar{Q}_{11} & \bar{Q}_{12} & \bar{Q}_{13} \\ \bar{Q}_{21} & \bar{Q}_{22} & \bar{Q}_{23} \\ \bar{Q}_{31} & \bar{Q}_{32} & \bar{Q}_{33} \end{bmatrix} \cdot \begin{bmatrix} \varepsilon_x^\circ \\ \varepsilon_y^\circ \\ \gamma_{xy}^\circ \end{bmatrix} + Z \cdot \begin{bmatrix} \bar{Q}_{11} & \bar{Q}_{12} & \bar{Q}_{13} \\ \bar{Q}_{21} & \bar{Q}_{22} & \bar{Q}_{23} \\ \bar{Q}_{31} & \bar{Q}_{32} & \bar{Q}_{33} \end{bmatrix} \cdot \begin{bmatrix} k_x \\ k_y \\ k_{xy} \end{bmatrix} \quad (10)$$

To find the force resultants acting on the total laminate, Equation (10) is integrated over the total thickness in the z direction.

$$\begin{bmatrix} N_x \\ N_y \\ N_{xy} \end{bmatrix} = \int_{-t/2}^{t/2} \begin{bmatrix} \sigma_x \\ \sigma_y \\ \tau_{xy} \end{bmatrix}_k \cdot dz = \sum_{k=1}^n \int_{z_{k-1}}^{z_k} \begin{bmatrix} \sigma_x \\ \sigma_y \\ \tau_{xy} \end{bmatrix} \cdot dz \quad (11)$$

$$\begin{bmatrix} M_x \\ M_y \\ M_{xy} \end{bmatrix} = \int_{-t/2}^{t/2} \begin{bmatrix} \sigma_x \\ \sigma_y \\ \tau_{xy} \end{bmatrix}_k \cdot z \cdot dz = \sum_{k=1}^n \int_{z_{k-1}}^{z_k} \begin{bmatrix} \sigma_x \\ \sigma_y \\ \tau_{xy} \end{bmatrix} \cdot z \cdot dz \quad (12)$$

After integration and rearranging equations (11 and 12), the constitutive equations can be obtained as follows:

$$\begin{bmatrix} N_x \\ N_y \\ N_{xy} \\ M_x \\ M_y \\ M_{xy} \end{bmatrix} = \begin{bmatrix} A_{11} & A_{12} & A_{13} & B_{11} & B_{12} & B_{13} \\ A_{21} & A_{22} & A_{23} & B_{21} & B_{22} & B_{23} \\ A_{31} & A_{32} & A_{33} & B_{31} & B_{32} & B_{33} \\ B_{11} & B_{12} & B_{13} & D_{11} & D_{12} & D_{13} \\ B_{21} & B_{22} & B_{23} & D_{21} & D_{22} & D_{23} \\ B_{31} & B_{32} & B_{33} & D_{31} & D_{32} & D_{33} \end{bmatrix} \cdot \begin{bmatrix} \varepsilon_x^\circ \\ \varepsilon_y^\circ \\ \gamma_{xy}^\circ \\ k_x \\ k_y \\ k_{xy} \end{bmatrix} \quad (13)$$

Where:

$$\begin{aligned} A_{ij} &= \sum_{k=1}^n [(\bar{Q}_{ij}) \cdot (z_k - z_{k-1})] \\ B_{ij} &= \frac{1}{2} \cdot \sum_{k=1}^n [(\bar{Q}_{ij}) \cdot (z_k^2 - z_{k-1}^2)] \\ D_{ij} &= \frac{1}{3} \cdot \sum_{k=1}^n [(\bar{Q}_{ij}) \cdot (z_k^3 - z_{k-1}^3)] \end{aligned}$$

3.Experimental Work

The experimental part was carried out in the field to determine experimentally the critical load on many specimens of the composite material of unidirectional glass fiber – epoxy matrix composite plates with different fiber angles and volume fraction of fiber as following:

$V_f = 10\%, 20\%, 30\%$ and 40%

$\theta = 0^\circ, 15^\circ, 30^\circ, 45^\circ, 60^\circ, 75^\circ, 90^\circ$

The dimension of the test specimen has a length of (200 mm) and width of (100 mm) and a thickness of (1mm).

Figure (2) represents the test machine with a test specimen of the

composite plate with some accessories like dial-gauge and load indicator to measure the lateral deflection of the composite plate.

4. Finite element Analysis

The finite element analysis carried out as part of this work was performed using the ANSYS package in the buckling analysis of composite plate to determine the critical load at which the structure becomes unstable.

Element Selected

This element is used to modal the composite plate. The element has six degrees of freedom at each node translation in the x,y and z directions and rotations about the nodal x,y and z-axes. The geometry, node locations, and the coordinate system for this element are shown in figure (3). The element is defined by eight nodes four thicknesses and orthotropic material properties [12].

5. Boundary Conditions And Mesh Generation

There are two main types of boundary condition (displacement and load boundary condition). The composite plate is a simply – supported plate from the two opposite edge and free from other edges and the load is applied axially on the two opposite edges.

As for the mesh generation of the composite plate, it is necessary to discretize it into a sufficient number of elements in order to obtain a reasonable accuracy.

Figure (4) represents the mesh generation and boundary conditions of the composite plate.

6. Results and Discussions

The results obtained from the experimental work and the finite element analyses of the buckling analysis of the composite plate are discussed here.

Figure (5) shows the lateral deflection contours and the value of the

critical load of the unidirectional composite plate at ($V_f = 10\%$)

It is clear from these figures that the buckling happens at the midline of the plane and the values of ($P_{cr} = 195.83$ N/m, 139.82 N/m, 73.111 N/m and 55.142 N/m) at fiber angle are ($\theta = 0^\circ$, 30° , 60° and 90°) respectively.

Figure (6) shows the relationship between the critical load and the fiber angle of the composite plate at different fiber volume fraction and at ($L/w = 2$) for the finite element analysis.

It is clear from this figure that the critical load decreases in nonlinear relationship with the increase of the fiber angle in different manners depending on the volume fraction. The maximum value of ($P_{cr} = 629.54$ N/m) at ($\theta = 0^\circ$ and $V_f = 40\%$) while the minimum value of ($P_{cr} = 55.142$ N/m) at ($\theta = 90^\circ$ and $V_f = 10\%$).

Figure (7) shows the relationship between the critical load and fiber volume fraction of the composite plate at different fiber angles for the finite element method.

It can be seen that the critical load increases with the increase of the fiber volume fraction in different manners depending on the fiber angle, where the behavior of curve at ($\theta = 0^\circ$) is the greatest one. At this angle the maximum value of ($P_{cr} = 629.54$ N/m) at ($V_f = 40\%$) while the minimum value of ($P_{cr} = 195.83$ N/m) at ($V_f = 10\%$).

Figure (8) shows the relationship between the critical load and the fiber angle of the composite plate at different fiber volume fractions and at ($L/w = 2$) for the experimental work.

It is clear from this figure that the critical load decreases in nonlinear relationship with the increase of the fiber angle in different manners depending on the volume fraction. The maximum value of ($P_{cr} = 560$ N/m) at ($\theta = 0^\circ$ and $V_f = 40\%$) while the minimum value of

($P_{cr} = 49 \text{ N/m}$) at ($\theta = 90^\circ$ and $V_f = 10 \%$).

Figure (9) shows the relationship between the critical load and the fiber volume fraction of the composite plate at different fiber angle for experimental work.

It can be seen that the critical load increases with the increase of the fiber volume fraction in different manners depending on the fiber angle, where the behavior of the curve at ($\theta = 0^\circ$) is the greatest one. At this angle the maximum value of ($P_{cr} = 560 \text{ N/m}$) at ($V_f = 40 \%$) while the minimum value of ($P_{cr} = 173 \text{ N/m}$) at ($V_f = 10 \%$).

Figure (10) shows the relationship between the critical load and the fiber angle at ($V_f = 40 \%$) and at ($L/w = 2$) for the experimental and finite element analysis.

It is clear from this figure that the critical load decreases in nonlinear relationship with the increase of the fiber angle. It has also been found that the maximum difference between the finite element analysis results and the experimental results (11 %) at ($\theta = 0^\circ$). The reason for this difference is attributed to the condition of preparing the specimens.

Figure (11) shows the relationship between the critical load and the fiber volume fraction at ($\theta = 0^\circ$) and at ($L/w = 2$) for the experimental and finite element analysis.

It is clear from this figure that the critical load increases in linear relationship with the increase of the fiber volume fraction and it has also been found that the maximum difference between finite element analysis results and experimental results (= 11 %) at ($V_f = 40 \%$).

7.Conclusion

The main conclusions of the buckling analysis of the composite plates for finite element analysis and the experimental work are:-

- (1-) Critical load decreases in nonlinear relationship with the increase of the fiber angle in different manners depending on the fiber volume fraction and the maximum value of ($P_{cr} = 629.54 \text{ N/m}$) at ($\theta = 0^\circ$) and ($V_f = 40 \%$) for finite element analysis.
- (2-) Critical load increases with the increase of the fiber volume fraction and the minimum value ($P_{cr} = 55.142 \text{ N/m}$) at ($\theta = 90^\circ$) and ($V_f = 10 \%$) for finite element analysis.
- (3-) The behavior of the critical load with fiber angle and with fiber volume fraction for experimental work is similar to the behavior of finite element analysis but here the maximum value of ($P_{cr} = 560 \text{ N/m}$) at ($\theta = 0^\circ$) and ($V_f = 40 \%$) the minimum value of ($P_{cr} = 49 \text{ N/m}$) at ($\theta = 90^\circ$) and ($V_f = 10 \%$).
- (4-) Maximum difference between the results of finite element analysis and experimental work results (= 11 %) at ($\theta = 0^\circ$) and ($V_f = 40 \%$).

8.References

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Notation

A_{ij}	Extensional stiffness terms (N/m).		force intensity in the xy-axis/unit width of the laminate cross-section (N).
B_{ij}	Coupling stiffness terms (N).	Q_{ij}	Reduced stiffness terms (N/m ²).
D_{ij}	Bending stiffness terms (N.m).	\bar{Q}_{ij}	Transformed reduced stiffness terms (N/m ²).
E_{11}	Young's modulus in the fiber direction (N/m ²).	$[Q]$	Reduced stiffness matrix.
E_{22}	Young's modulus in the matrix direction (N/m ²).	$[\bar{Q}]$	Transformed reduced stiffness matrix.
E_f	Young's modulus of the fiber (N/m ²).	V_f	Volume fraction of fiber (%).
E_m	Young's modulus of the matrix (N/m ²).	V_m	Volume fraction of matrix (%).
G_{12}	Shear Modulus along the principal axis (N/m ²).	z	Coordinate measured from the midplane (m).
k_x, k_y, k_{xy}	Curvatures of the midplane (m).	$\varepsilon_x^\circ, \varepsilon_y^\circ, \gamma_{xy}^\circ$	Midplane strains.
M_x	Resultant moment intensity about the y-axis per unit width of the laminate cross-section (N.m).	$\underline{\varepsilon}$	Strain vector in ply.
M_y	Resultant moment intensity about the x-axis per unit width of the laminate cross-section (N.m).	$\underline{\sigma}$	Stress vector in ply.
M_{xy}	Resultant twisting moment intensity about the xy-axis/unit width of the laminate cross-section (N.m).	σ_i	Stress components (N/m ²).
N_x	Resultant in-plane force intensity in the x-axis/unit width of the laminate cross-section (N).	τ_{12}	Shear strength along the principal axis (N/m ²)
N_y	Resultant in-plane force intensity in the y-axis/unit width of the laminate cross-section (N).	γ_{12}	Shear strain along the principal axis.
N_{xy}	Resultant in-plane shearing	θ	Fiber angle (°).
		ν_{12}, ν_{21}	Major and Minor poisson's ratio.

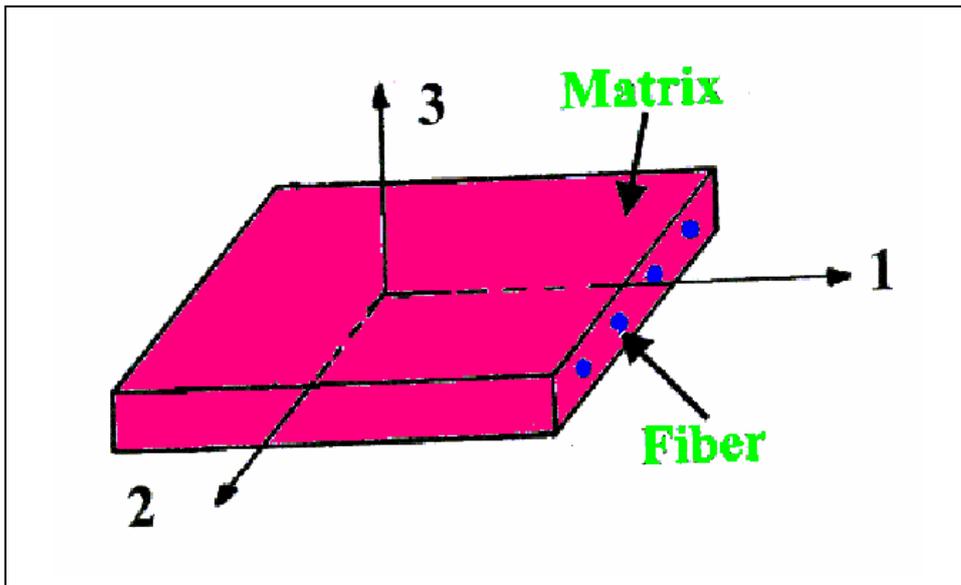


Figure (1): Location of Material (Principal) Coordinate System on the Lamina [11].

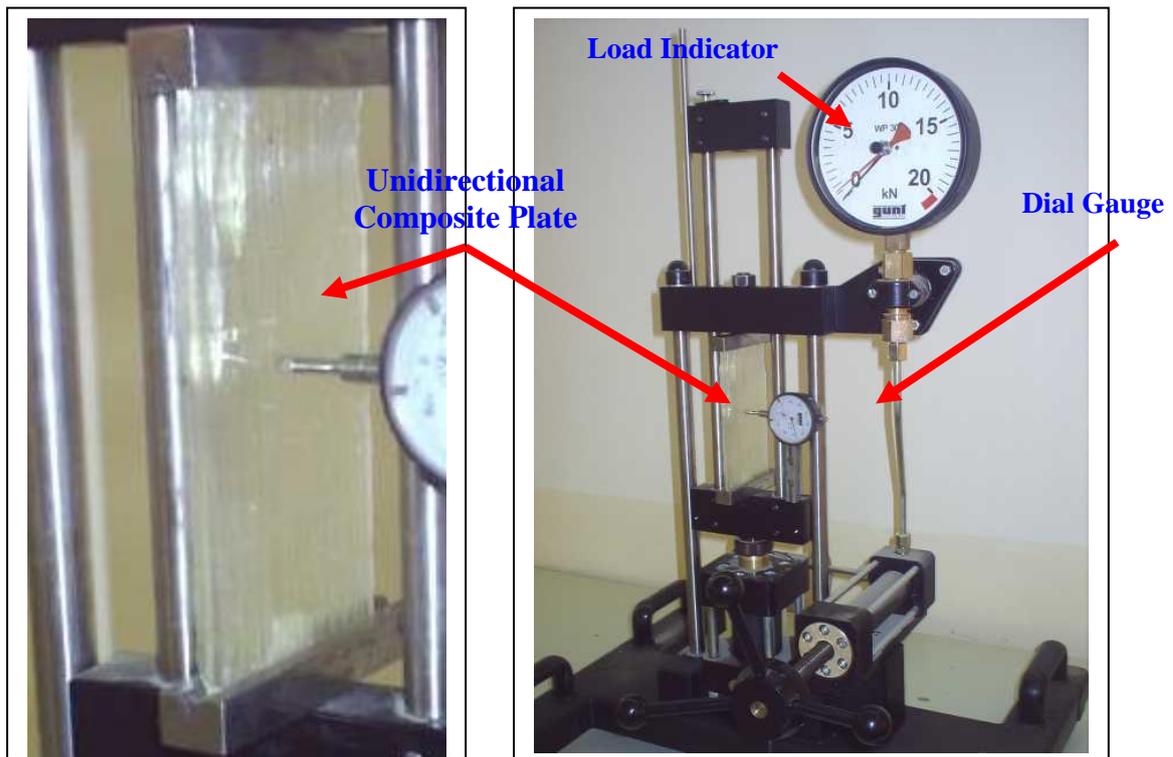


Figure (2): Test Apparatus and Test Specimen

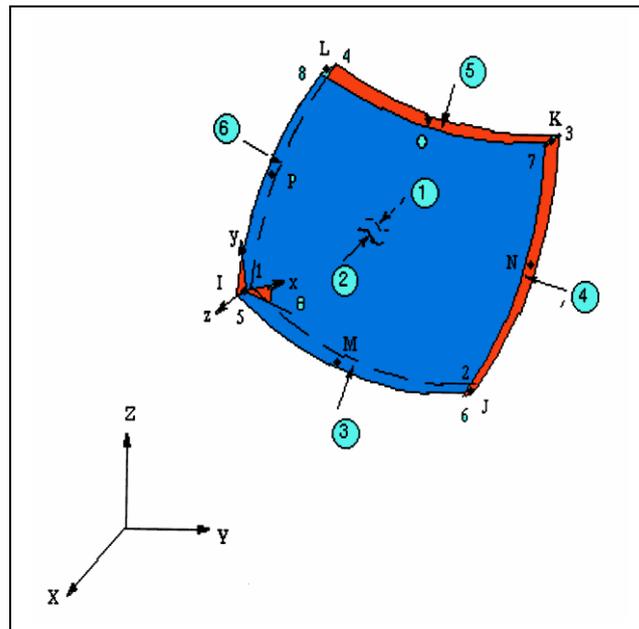


Figure (3) : SHELL93 8-Node Structural Shell [12].

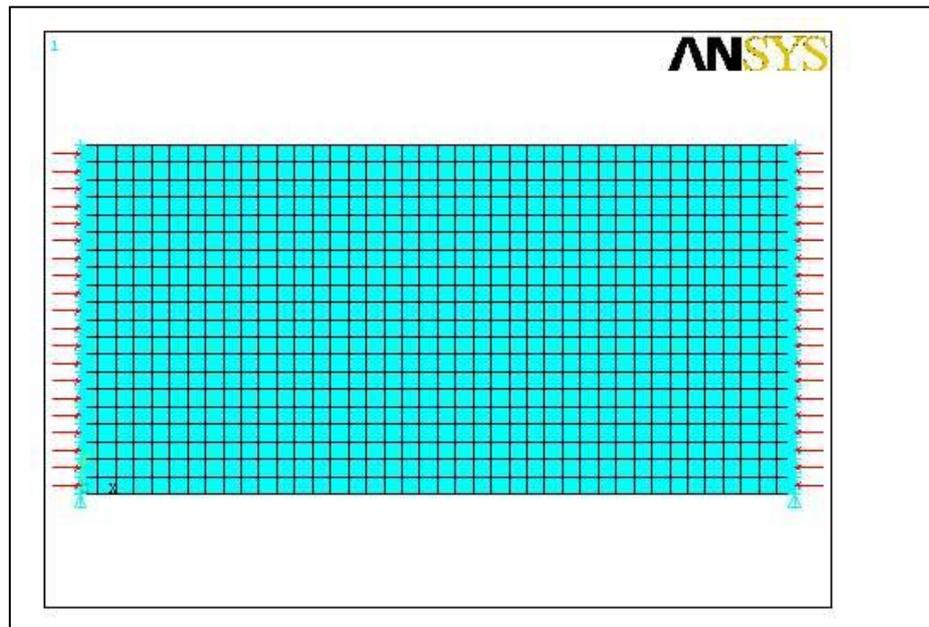


Figure (4) : Mesh Generation and Boundary Conditions of the Composite Plate.

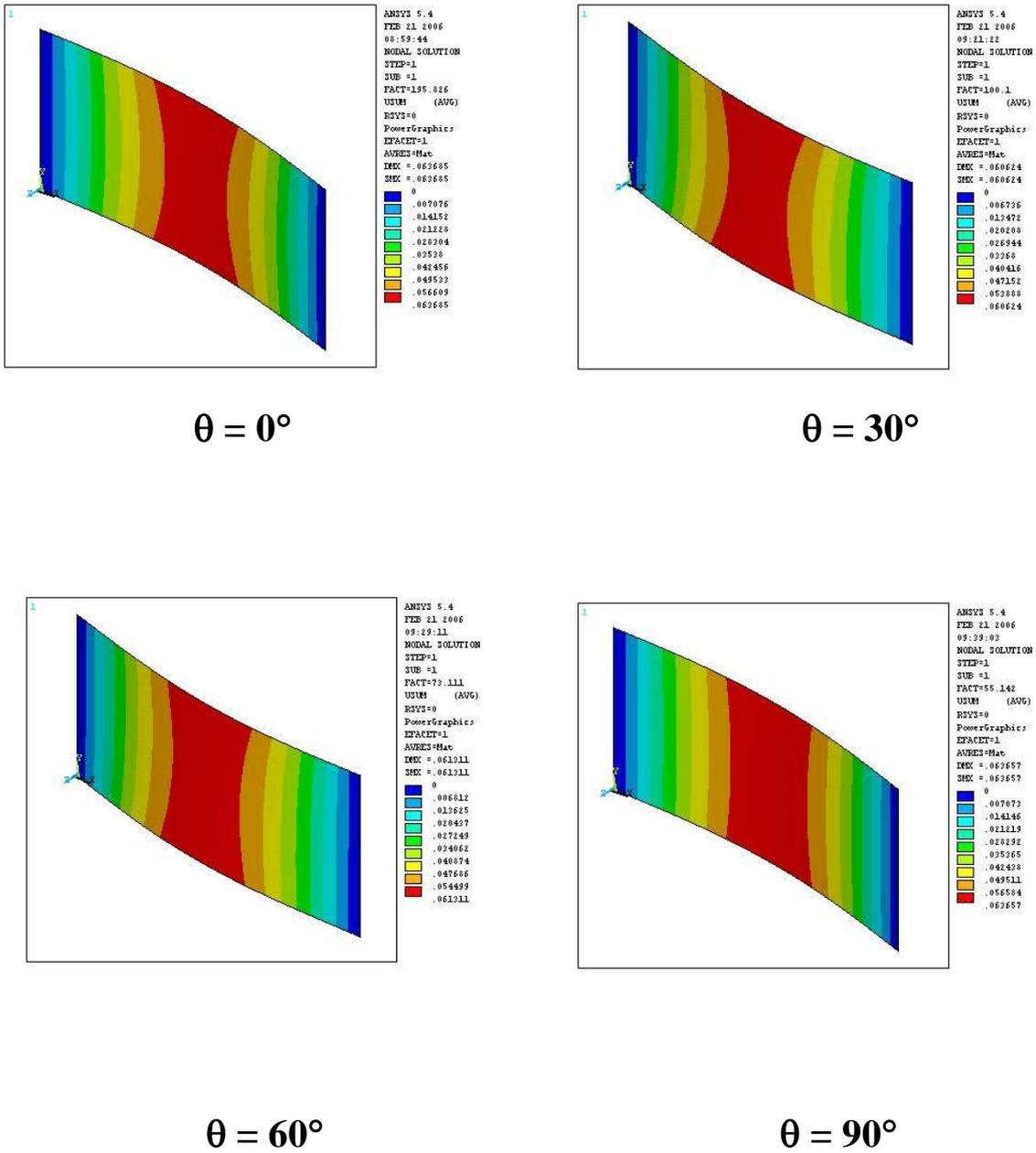


Figure (5): Deflection Contours of the Composite Plates at ($V_f=10\%$) and at Different Value of Fiber Angle.

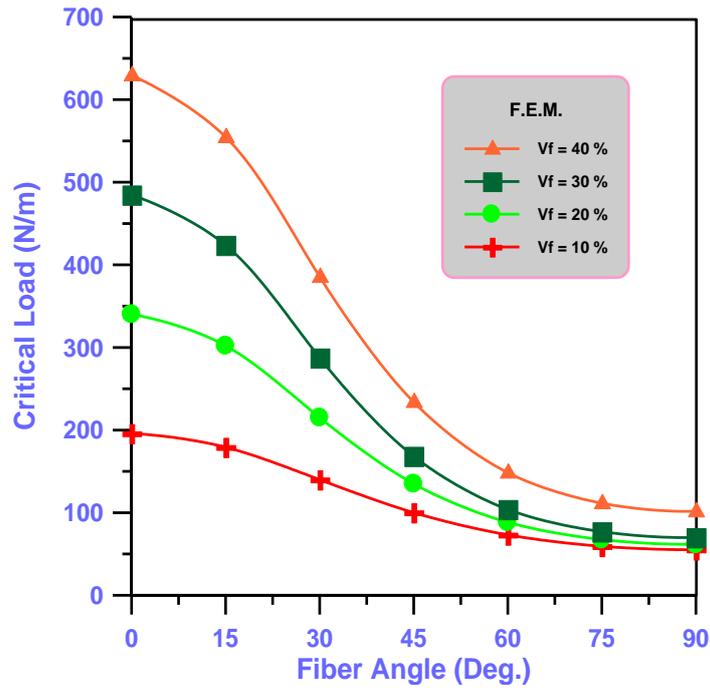


Figure (6): Relationship Between Critical Load and Fiber Angle for Finite Element Analysis at Different Volume Fraction.

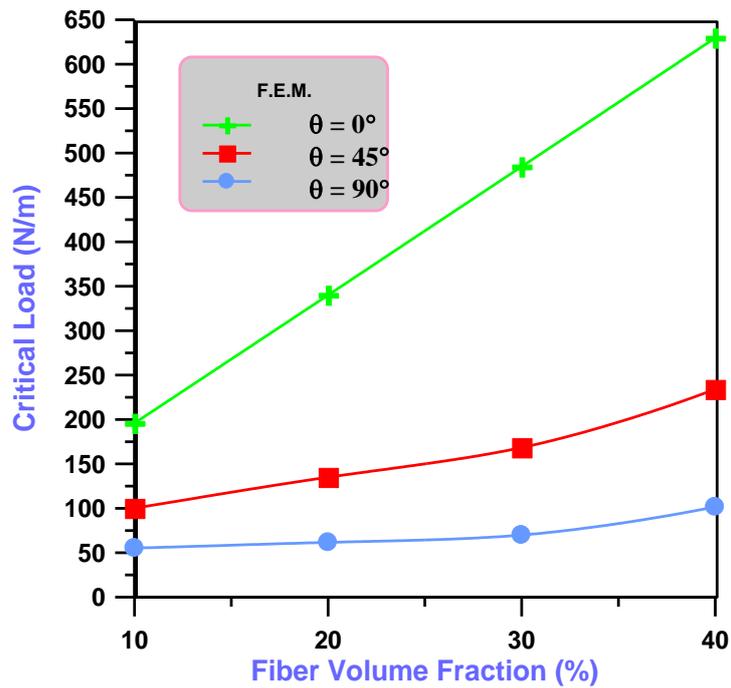


Figure (7): Relationship Between Critical Load and Fiber Volume Fraction for Finite Element Analysis at Different Fiber Angle.

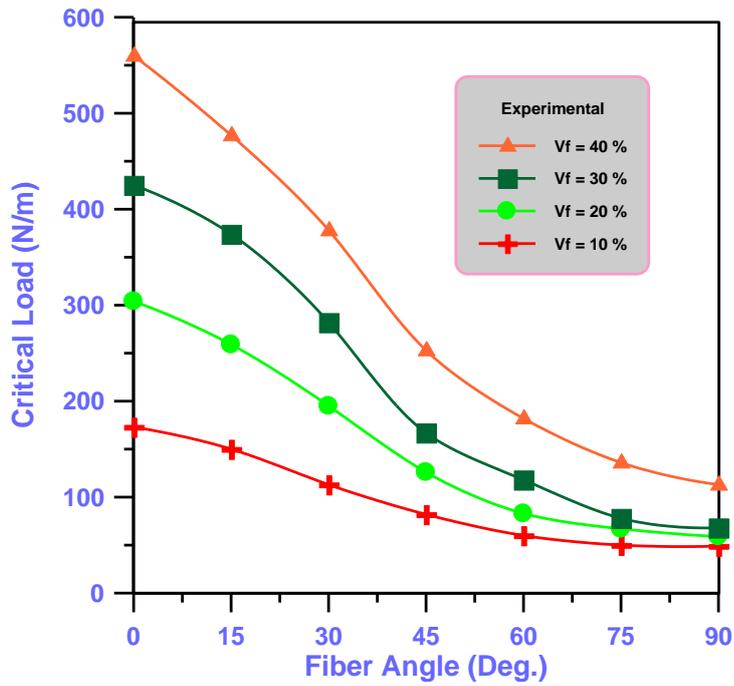


Figure (8) : Relationship Between Critical Load and Fiber Angle for Experimental at Different Volume Fraction.

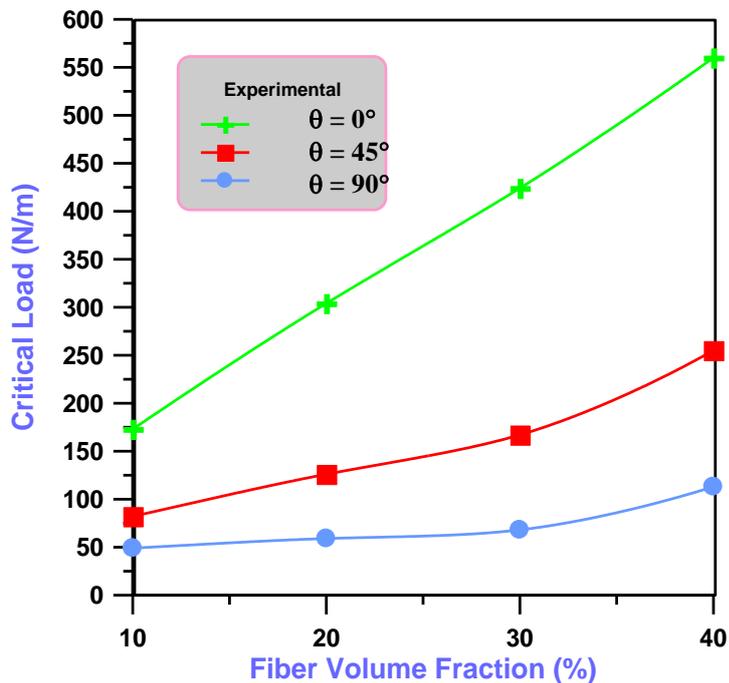


Figure (9) : Relationship Between Critical Load and Fiber Volume Fraction for Experimental at Different Fiber Angle.

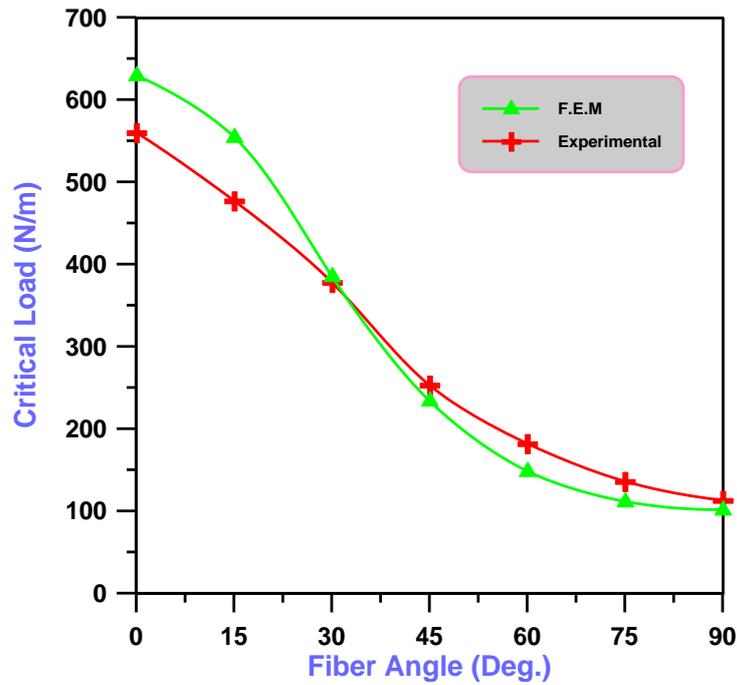


Figure (10): Relationship Between Critical Load and Fiber Angle for Finite Element Analysis Experimental at Fiber Volume Fraction(= 40 %).

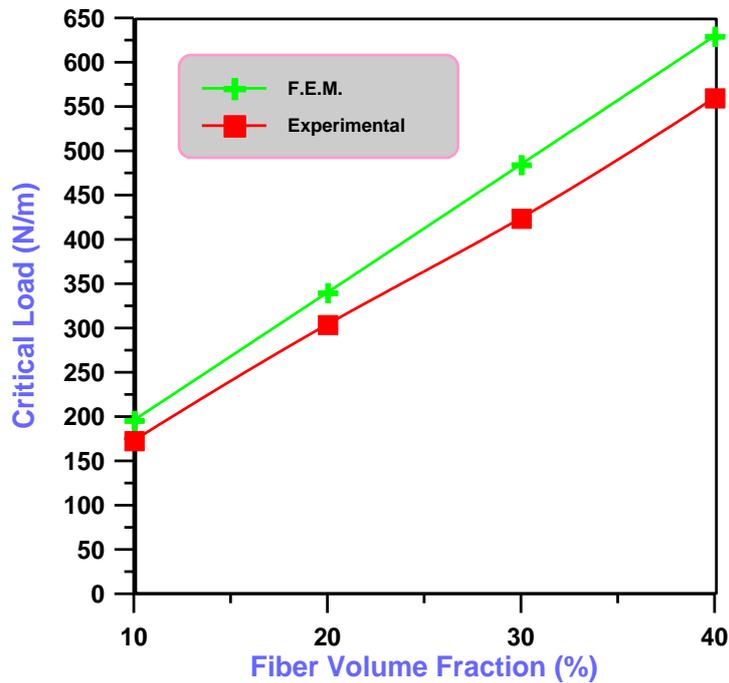


Figure (11): Relationship Between Critical Load and Fiber Volume Fraction for Finite Element Analysis and Experimental at Fiber Angle (= 0°).

تحليل الأنبعاج للصفائح المركبة الأحادية الاتجاه ذات الأساس البوليمري

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الخلاصة:

تهتم هذه الدراسة بتقييم الحمل الحرج للصفائح المركبة الأحادية الاتجاه ذات الأساس البوليمري باستخدام الطريقة العملية وطريقة تقنيات العناصر المحددة عند زوايا ليف مختلفة وكسر حجمي مختلف لتلك الصفائح.

أذ يبين تحليل الأنبعاج بان الحمل الحرج يقل بعلاقة غير خطية مع زيادة زاوية الليف ويزداد مع زيادة الكسر الحجمي للليف.

بينت النتائج بان اقصى قيمة للحمل الحرج لكل وحدة طول ($P_{cr} = 629.5 \text{ N/m}$) عند ($\theta = 0^\circ$) و ($V_f = 40\%$) لطريقة العناصر المحددة. بينما اقل قيمة للحمل الحرج ($P_{cr} = 49 \text{ N/m}$) عند ($\theta = 90^\circ$) و ($V_f = 10\%$) للطريقة العملية.

وكذلك بينت النتائج بان اقصى فرق بين طريقة العناصر المحددة والطريقة العملية ($= 11\%$) عند ($\theta = 0^\circ$) و ($V_f = 40\%$).